# **Sky Reconstruction from Cylinder Visibilities**

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#### Visibility

This note will consider the reconstruction of the sky from the measured visibilities from a pair of cylinder antenna arrays. It is assumed that the cylinders fixed and are oriented along the meridian. Each cylinder is populated with N feeds spaced uniformly along the length. The output voltage of each feed provides an input of a spatial Fourier transform along the cylinder length. The spatial Fourier transform forms N beams along the length of the cylinder.

For a pair of cylinders the visibility between cylinders is formed for each beam. As the sky drifts through the cylinder beam, the visibility for beam  $\mathbf{k}$  is:

$$v_k(\varphi) = \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} \frac{\tilde{A}_k(\theta, \phi)}{\lambda^2} T(\theta, \varphi - \phi) \cos(\theta) \, d\theta d\phi \tag{1}$$

Where  $\varphi$  is the time of the day (in units of angle),  $\lambda$  is the wavelength and T is the power flux of the sky. The cylinder pair Fourier area is defined as

$$\tilde{A}_{k}(\theta,\phi) = \tilde{\mathbf{a}}_{k,c1}(\theta,\phi) \left( \tilde{\mathbf{a}}_{k,c2}(\theta,\phi) \right)^{*}$$
(2)

where the subscripts **c1**, **c2** indicate cylinder 1 and cylinder 2, respectively. The Fourier root area of a cylinder is defined as

$$\tilde{\mathbf{a}}_{\mathbf{k},\mathbf{c}}(\theta,\phi) = \sum_{n} \mathbf{a}_{\mathbf{n}}(\theta,\phi) e^{-j\vec{\beta}(\theta,\phi)\cdot\vec{r}_{n,c}} e^{j2\pi k\frac{n}{N}}$$
(3)

Where **n** is the feed number,  $\mathbf{r}_{n,c}$  is the global location of the feed and  $\boldsymbol{\beta}$  is the incoming wave vector:

$$\vec{\beta}(\theta,\phi) = \frac{2\pi}{\lambda} (\sin(\theta)\hat{x} + \cos(\theta)\sin(\phi)\hat{y}) \tag{4}$$

It is assumed that the length of the cylinders is in the x direction.

# Sky Expansion

Since the sky is periodic in right ascension, it can be expanded in a Fourier series:

$$T(\theta,\phi) = \sum_{l} \chi_{l}(\theta) \left( \tilde{T}_{dc_{l,0}} + \sum_{m} \tilde{T}_{c_{l,m}} cos(m\phi) + \sum_{m} \tilde{T}_{s_{l,m}} sin(m\phi) \right)$$
 (5)

Substituting Equation 5 into Equation 1,

$$\begin{split} ℜ\{v_{k}(\varphi)\}\\ &= \sum_{l} \hat{A}_{dc\ k,l,0}^{(R)} \tilde{T}_{l,0}\\ &+ \sum_{l} \sum_{m} \hat{A}_{c\ k,l,m}^{(R)} \tilde{T}_{cl,m} cos(m\varphi) - \sum_{l} \sum_{m} \hat{A}_{s\ k,l,m}^{(R)} \tilde{T}_{sl,m} cos(m\varphi)\\ &+ \sum_{l} \sum_{m} \hat{A}_{s\ k,l,m}^{(R)} \tilde{T}_{cl,m} sin(m\varphi) + \sum_{l} \sum_{m} \hat{A}_{c\ k,l,m}^{(R)} \tilde{T}_{sl,m} sin(m\varphi) \end{split} \tag{6}$$

where:

$$\hat{A}_{dc}^{(R)}_{k,l,0} = \int_{-\pi}^{\pi} \int_{-\pi}^{\pi} \frac{Re\{\tilde{A}_k(\theta,\phi)\}}{\lambda^2} \chi_l(\theta) cos(\theta) d\theta d\phi$$
(7)

$$\hat{A}_{c}^{(R)}{}_{k,l,m} = \int_{-\pi}^{\pi} cos(m\phi) \int_{-\pi}^{\pi} \frac{Re\{\tilde{A}_{k}(\theta,\phi)\}}{\lambda^{2}} \chi_{l}(\theta) cos(\theta) d\theta d\phi$$
(8)

$$\hat{A}_{s}^{(R)}{}_{k,l,m} = \int_{-\pi}^{\pi} \sin(m\phi) \int_{-\pi}^{\pi} \frac{Re\{\tilde{A}_{k}(\theta,\phi)\}}{\lambda^{2}} \chi_{l}(\theta) \cos(\theta) \, d\theta \, d\phi \tag{9}$$

## Fourier Transform of Cylinder Visibilities

Now assume that the visibility is measured at N discrete times during the day. The visibility will be periodic with a period of a day so we can expand the visibility into a Fourier series.

$$Re\{v_{k}(\varphi_{n})\} = \tilde{V}_{dc}^{(R)}{}_{k,0} + \sum_{m'} \tilde{V}_{c}^{(R)}{}_{k,m'} cos(m'\varphi_{n}) + \sum_{m'} \tilde{V}_{s}^{(R)}{}_{k,m'} sin(m'\varphi_{n})$$
(10)

where

$$\tilde{V}_{dc_{k,0}}^{(R)} = \frac{1}{N} \sum_{n} Re\{v_k(\varphi_n)\}$$
 (11)

$$\tilde{V}_{c}^{(R)}_{k,m'} = \frac{2}{N} \sum_{n} Re\{v_k(\varphi_n)\} \cos(m'\varphi_n)$$
(12)

$$\tilde{V}_{s}^{(R)}_{k,m'} = \frac{2}{N} \sum_{n} Re\{v_k(\varphi_n)\} \sin(m'\varphi_n)$$
(13)

Substituting Equations 6 into Equations 8, 9, 10,

$$\tilde{V}_{dc\ k,0}^{(R)} = \sum_{l} \hat{A}_{dc\ k,l,0}^{(R)} \tilde{T}_{l,0}$$
(14)

$$\tilde{V}_{c}^{(R)}{}_{k,m} = \sum_{l} \hat{A}_{c}^{(R)}{}_{k,l,m} \tilde{T}_{cl,m} - \hat{A}_{s}^{(R)}{}_{k,l,m} \tilde{T}_{sl,m}$$
(15)

$$\tilde{V}_{s}^{(R)}_{k,m} = \sum_{l} \hat{A}_{s}^{(R)}_{k,l,m} \tilde{T}_{cl,m} + \hat{A}_{c}^{(R)}_{k,l,m} \tilde{T}_{sl,m}$$
(16)

## Sky Mode Matrix Equations

Equation 15 and 16 can be combined if we write:

$$\tilde{V}^{(R)}_{k,m} = \tilde{V}_{c}^{(R)}_{k,m} - j\tilde{V}_{s}^{(R)}_{k,m} \tag{17}$$

$$\hat{A}^{(R)}_{k,l,m} = \hat{A}_{c}^{(R)}_{k,l,m} - j\hat{A}_{s}^{(R)}_{k,l,m} \tag{18}$$

$$\tilde{T}_{l,m} = \tilde{T}_{c_{l,m}} - j\tilde{T}_{s_{l,m}} \tag{19}$$

Then:

$$\tilde{V}^{(R)}{}_{k,m} = \sum_{l} \hat{A}^{(R)}{}_{k,l,m} \tilde{T}_{l,m} \tag{20}$$

where:

$$\tilde{V}^{(R)}_{k,m} = \frac{2}{N} \sum_{n} Re\{v_k(\varphi_n)\} e^{-jm\varphi_n}$$
(21)

$$\hat{A}_{c}^{(R)}{}_{k,l,m} = \int_{-\pi}^{\pi} e^{-jm\phi} \int_{-\pi}^{\pi} \frac{Re\{\tilde{A}_{k}(\theta,\phi)\}}{\lambda^{2}} \chi_{l}(\theta) cos(\theta) d\theta d\phi$$
(22)

$$T(\theta,\phi) = \sum_{l} \chi_{l}(\theta) \left( \tilde{T}_{dc_{l,0}} + Re \left\{ \sum_{m} \tilde{T}_{c_{l,m}} e^{jm\phi} \right\} \right)$$
 (23)

## Discussion on Sign Convention

Since the sky temperature must be a real function, in Equation 5, we expanded the sky temperature in a real Fourier series. Since the choice of which cylinder is first in the definition of the visibility in Equation 2 is arbitrary, the choice of coordinate system for the incoming wave vector in Equation 3 and 4, and the choice of sign for the mode number m in Equation 5 is will change the signs of the imaginary part of the Fourier transform of the visibility. For example, if the  $\mathbf{y}$  location of cylinder 2 is **greater** than cylinder 1, then for an ideal pair of cylinders:

$$\hat{A}^{(R)}_{k,l,m} = \hat{A}^{(R)}_{k,l,-m} = j\hat{A}^{(l)}_{k,l,m} = -j\hat{A}^{(l)}_{k,l,-m}$$
(24)

However, if the y location of cylinder 2 is **less** than cylinder 1, then for an ideal pair of cylinders then:

$$\hat{A}^{(R)}_{k,l,m} = \hat{A}^{(R)}_{k,l,-m} = -j\hat{A}^{(I)}_{k,l,m} = j\hat{A}^{(I)}_{k,l,-m}$$
(25)

If one is not careful with the choice of sign of the sky expansion mode number m and the choice of definition of which cylinder visibility, the complex Fourier transform can be matrix element  $A_{k,l,m}$  can be zero. For these reasons, the choice of only using the Fourier transform of the real part of the visibilities in Equation 10 was decided.